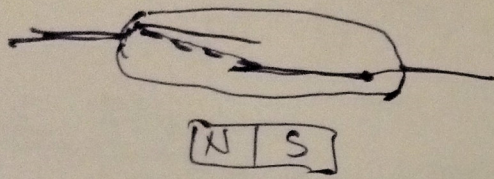


Reed switch:



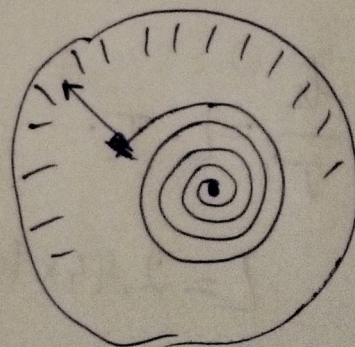
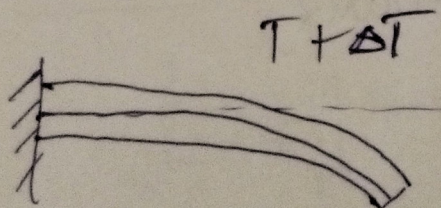
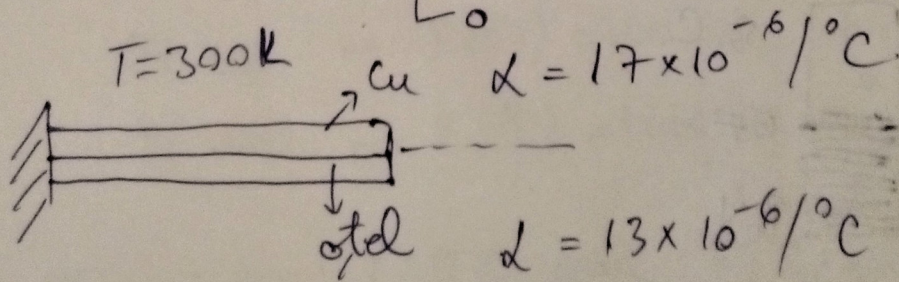
Senzori de temperatura:

$$\frac{\Delta L}{L_0}(T); \rho(T); t.e.m(T); \epsilon_r(T); \Delta Q(\Delta T).$$

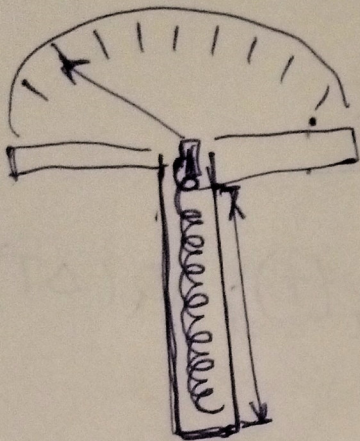
Termometru bimetalic:

$$\alpha_v = \frac{1}{v} \cdot \left(\frac{\partial v}{\partial T} \right)_{p=ct}$$

liniar $\frac{\Delta L}{L_0} = \alpha \cdot \Delta T$



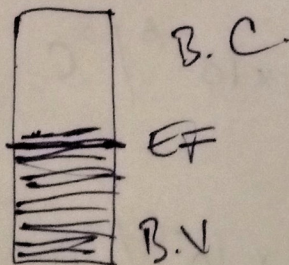
-30° - 500°C



Termometre resistive

RTD.

Resistance temperature detector.



Leges Wiedemann-Franz.

$$\frac{k}{\sigma} = L \cdot T$$

$$L = 2.44 \times 10^{-8} \text{ W } \Omega \text{ K}^{-2}$$

$$f = f_0 (1 + \alpha \cdot (T - T_0))$$

$$f_0 = f_1(T_0)$$

•) Pt. Pt100:
 $-200^\circ\text{C} \leq T \leq \text{~~0~~ } 0^\circ\text{C}$

$$f(T) = f_0 (1 + A \cdot T + B T^2 + C (T - 100) \cdot T^3)$$

•) $0^\circ\text{C} \leq T \leq 850^\circ\text{C}$

$$f(T) = f_0 (1 + A \cdot T + B T^2)$$

Pt100: $A = 3.90802 \times 10^{-3} \text{ } ^\circ\text{C}^{-1}$

$B = -5.80195 \times 10^{-7} \text{ } ^\circ\text{C}^{-2}$

$C = -4.2735 \times 10^{-12} \text{ } ^\circ\text{C}^{-4}$

Pt 100 $\rightarrow R(0^\circ\text{C}) = 100 \ \Omega$
 Pt 1000 $\rightarrow R(0^\circ\text{C}) = 1000 \ \Omega$

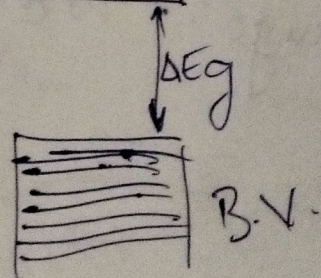
$\begin{cases} \rightarrow 2 \text{ wire} \\ \rightarrow 3 \text{ wire} \\ \rightarrow 4 \text{ wire} \end{cases}$

•) Termistori (NTC sau PTC):



la $T=0 \ \Gamma \sim 0$

$T \uparrow \ \Gamma \uparrow$



$$f = f_0 e^{-\alpha T}$$

Ecuatia Steinhart - Hart.

$$\frac{1}{T} = A + B \ln f + C \ln f^3$$

$$A = \frac{1}{T_0} - \frac{1}{B} \ln f_0.$$

$$B = \frac{1}{\beta}.$$

$$C = 0.$$

$$\frac{1}{T} = \frac{1}{T_0} + \frac{1}{\beta} \ln \frac{R}{R_0}.$$

$$R = R_0 e^{\beta \left(\frac{1}{T} - \frac{1}{T_0} \right)}.$$

$$R_0 = R(T_0)$$

$$T_0 = 25^\circ \text{C}.$$

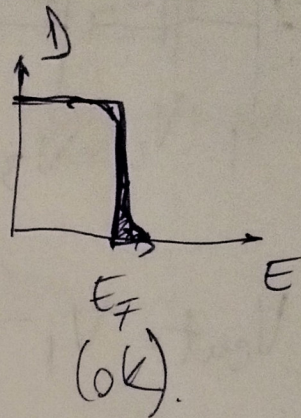
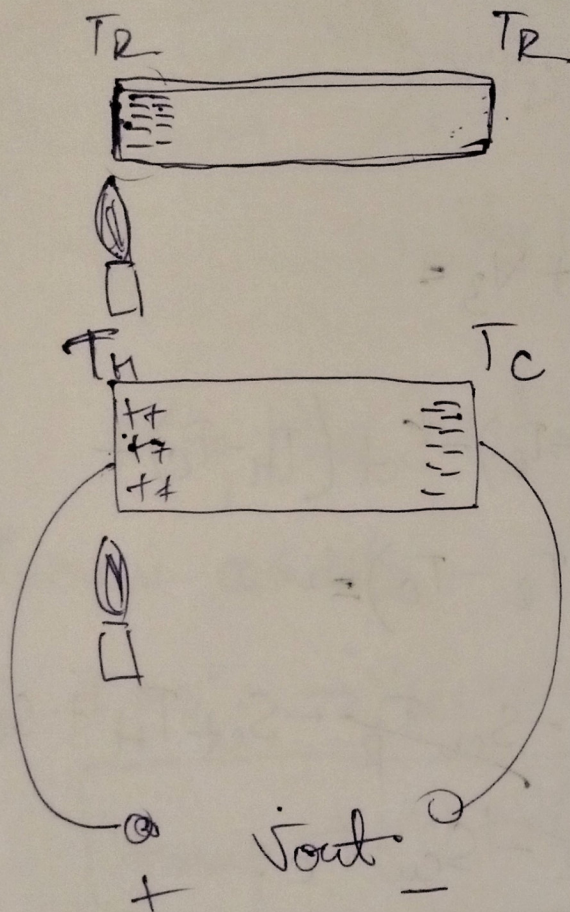
$$R = R_0 e^{\frac{\beta}{T}}$$

$$R_0 = R_0 e^{-\frac{\beta}{T_0}}$$

range: $-40^\circ \text{C} - 125^\circ \text{C}$

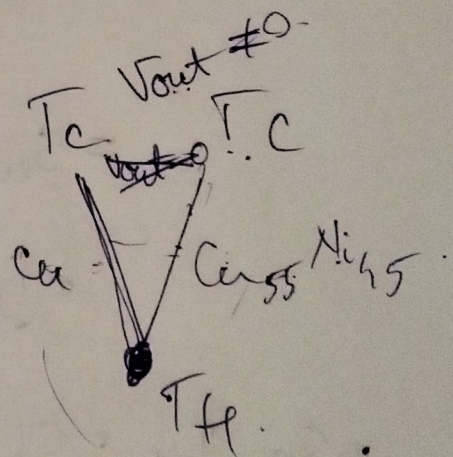
Thermocouple:

1) effect of Seebeck:

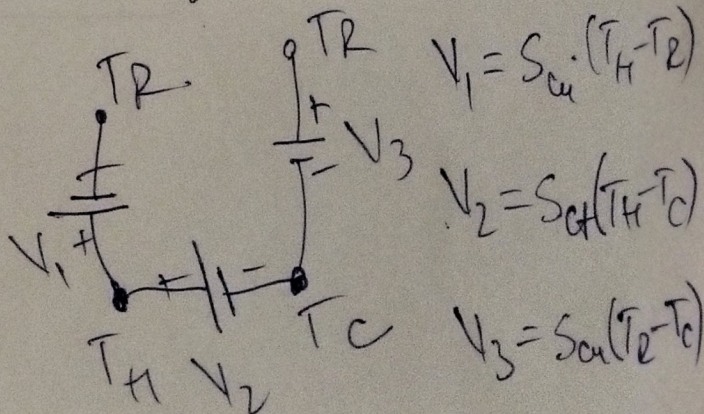
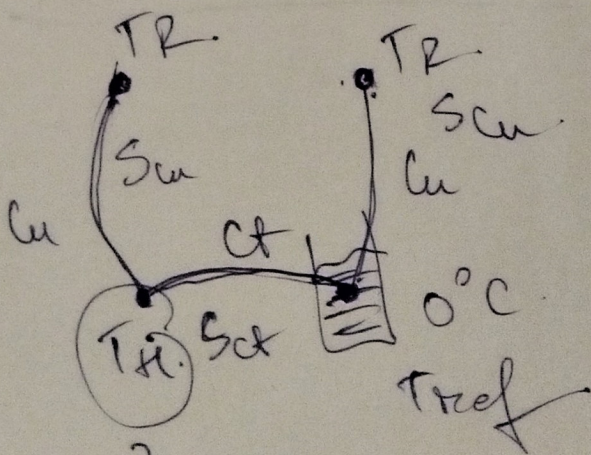
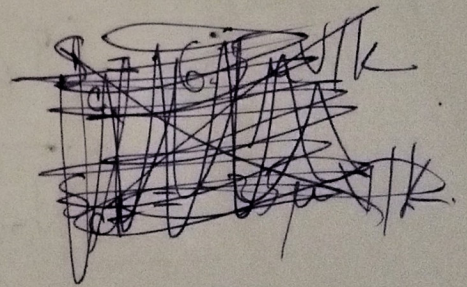


$$\Delta T = T_H - T_C$$

$$\Delta V = \int_{T_C}^{T_H} S(T) dT$$



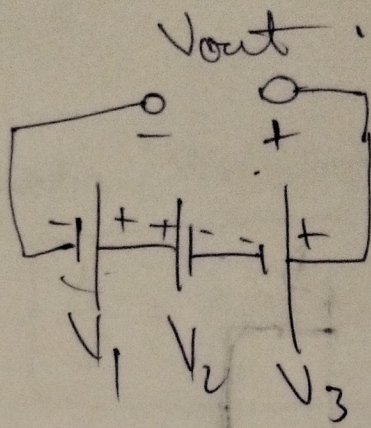
$$S = \left. \frac{\Delta V}{\Delta T} \right|_{I=0}$$



$$V_1 = S_{Cu} (T_H - T_C)$$

$$V_2 = S_{TR} (T_H - T_C)$$

$$V_3 = S_{Cu} (T_C - T_H)$$



$$V_{out} = V_1 - V_2 + V_3 =$$

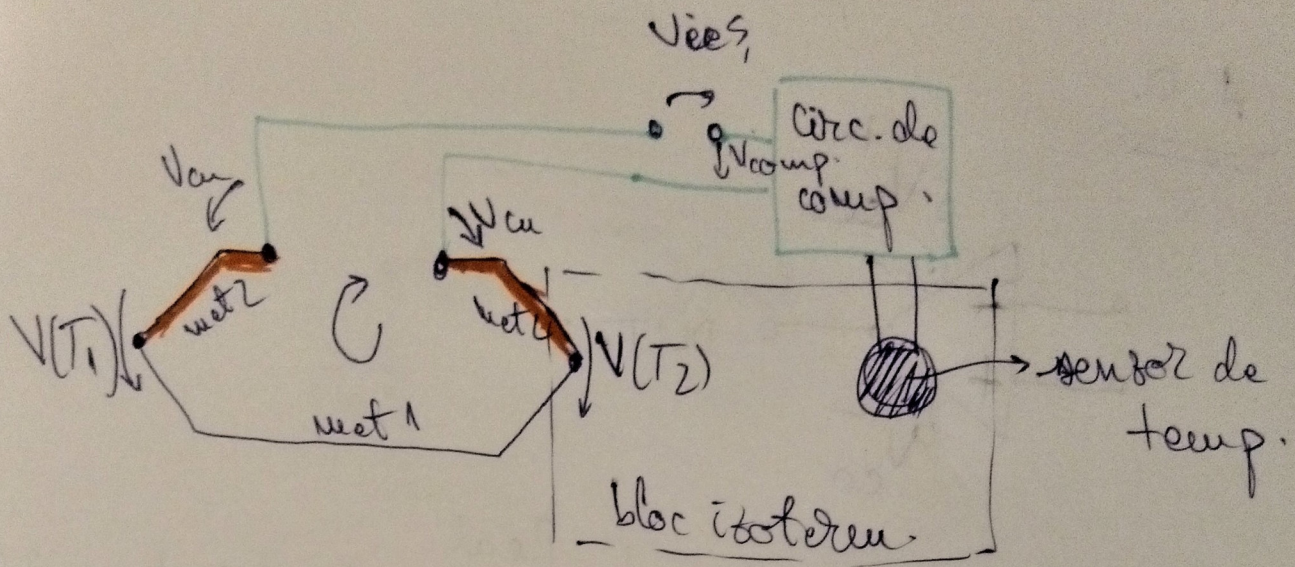
$$= S_{cu}(T_H - T_R) - S_{cf}(T_H - T_C) + S_{cu}(T_R - T_C) =$$

$$= S_{cu} \cdot T_H - \cancel{S_{cu} T_R} - S_{cf} T_H + S_{cf} \cdot T_C + \cancel{S_{cu} T_R} - S_{cu} \cdot T_C.$$

$$= S_{cu} T_H - S_{cu} \cdot T_C - S_{cf} \cdot T_H + S_{cf} \cdot T_C =$$

$$= S_{cu} \cdot (T_H - T_C) - S_{cf} (T_H - T_C) =$$

$$\Rightarrow \boxed{V_{out} = (S_{cu} - S_{cf})(T_H - T_C)}$$



$$V_{ies} + V_{cu} + V_{comp} + V(T_2) - V(T_1) - V_{cu} = 0.$$

Punem conditia:

Daca $T_1 = 0^\circ C \rightarrow V_{ies} = 0^\circ C$

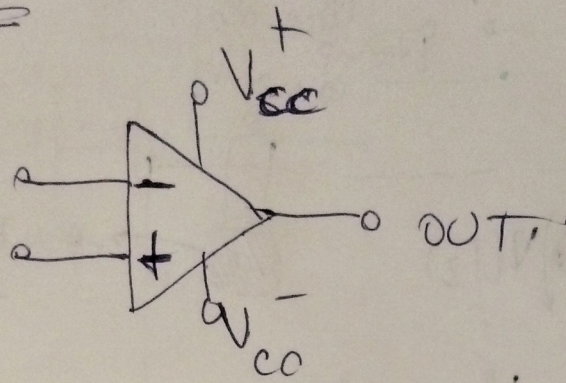
$$V_{comp} - V(0^\circ C) + V(T_2) = 0 \Rightarrow$$

$$\Rightarrow V_{comp} = -V(T_2) + V(0^\circ C)$$

$$V_{ies} - V(T_2) + V(0^\circ C) + V(T_2) - V(T_1) = 0$$

$$V_{ies} = V(T_1) - V(0^\circ C)$$

A.O.



A.O. ideal

$$f_{im} \rightarrow \infty$$

$$f_{out} \rightarrow 0$$

$$A_v \rightarrow \infty$$

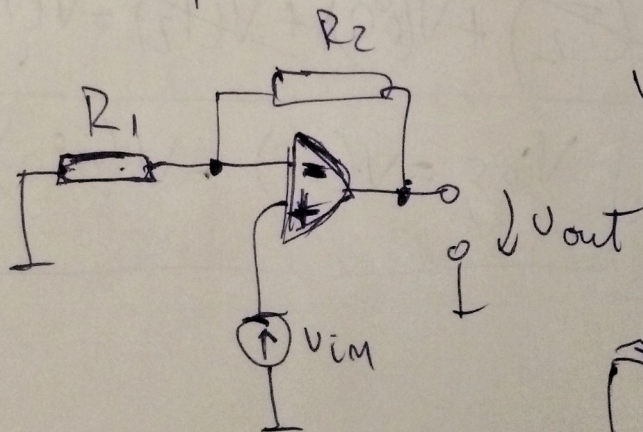
$$v_{out} = (v_+ - v_-) \cdot A_v$$

Real

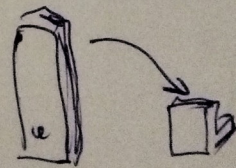
BJT $f_{im} \approx 200k\Omega - 2M\Omega$

FET $f_{im} \approx 10^{12} \Omega$

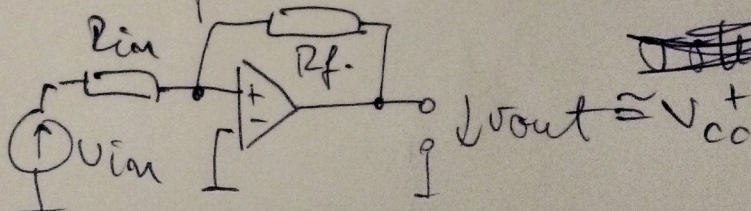
Negative feedback.



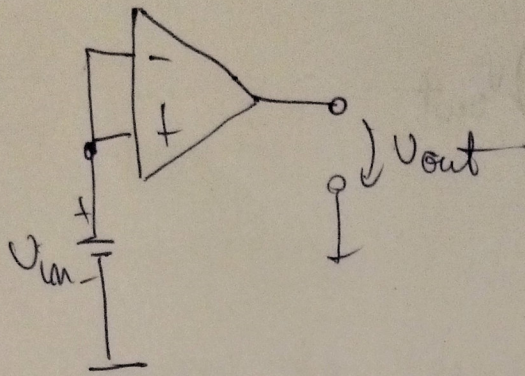
$$v_{out} = \left(1 + \frac{R_2}{R_1}\right) \cdot v_{in}$$



Positive feedback:



common-mode gain:



$$A_{v}^{cm} = \frac{\Delta v_{out}}{\Delta v_{in}} = 0 \text{ ideal}$$

$$CMRR = \frac{A_v}{A_v^{cm}} \text{ [dB]}$$

